

Communication

The Sliding-Aperture Transform and Its Applicability to Deep-Level Transient Spectroscopy

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Featured Application: Deep-level transient spectroscopy; any applications requiring extraction of rate and initial value of decaying exponentials.

Abstract: A mathematical method is presented for the extraction of defect parameters from the multiexponential decays generated during deep-level transient spectroscopy experiments. Such transient phenomenon results from the ionization of charge trapped in defects located in the depletion width of a semiconductor diode. From digitized transients acquired at fixed temperatures, this method produces a rate–domain spectral signature associated with all defects in the semiconductor. For signal-to-noise ratio of 1000, defect levels with carrier emission rates differing by as little as 1.5 times may be distinguished.

Keywords: DLTS; transient analysis; emission rate; extraction; curve fitting



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1. Introduction

Exponential transients are common in nature. The decay rates and initial values of these transients offer valuable insight into the underlying physics of their source. In semiconducting systems, both optical and electrical transients are used to characterize both bulk material and discrete devices. Deep-level transient spectroscopy (DLTS) is an experimental technique which analyzes exponentially decaying capacitance transients resulting from the emission of trapped charges from defects found in the depletion region of a diode [1]. Methods used to extract pertinent results from these transients are the basis of this and other works [1–7].

Semiconductor-based components in harsh environments, such as infrared sensors in space, accumulate electrically active defects due to radiation damage [8–14]. Such defects act as recombination and charge compensation centers and thereby affect minority carrier lifetime and free carrier concentration, which degrade circuit functionality. The ability to observe and understand the formation, evolution, and mitigation of defects in semiconductors is essential to prolonging the useful life of electronics and optoelectronics in harsh environments [15–17]. Accuracy and the ability to resolve closely spaced energy levels are important for a fundamental understanding of these defects. This paper presents an improved technique for analyzing capacitance transients at constant stable temperatures. The technique allows defect-level determination with higher accuracy and resolution than current approaches.

2. Methods

To investigate defects in semiconducting systems, the ionization or emission rate of trapped carriers $R(T)$ is typically used, and is given by

$$R(T) = P T^2 \exp\left[-\frac{E}{k_b T}\right], \tag{1}$$

where T is temperature and k_b is Boltzmann’s constant. The ionization energy, E , and the capture parameter, P , are unique defect-specific signatures, both required for an a priori determination of emission rate at a specific temperature. If the capture parameter and ionization energy are not known a priori, then the emission rate must be determined as a function of temperature. Once obtained, the capture parameter and ionization energy are extracted using Arrhenius analysis of $R(T)$ [1,18].

In practice, a capacitance transient is obtained by collapsing a diode’s depletion region for a time, t_{fill} , filling the defect sites with carriers [19]. A reverse bias is then applied at $t = 0$ to expand the depletion region and initiate defect ionization at rates determined by the ionization energy and capture parameter in Equation (1). Changes to diode capacitance occur as the diode depletion width expands or contracts to maintain charge neutrality in the depletion region of the diode as defect ionization occurs. This fill-and-measure sequence produces a capacitance transient, as shown in Figure 1, with the initial value $\pm C$, with respect to a steady state value B . The capacitance transient is of the form

$$C(t, T) = B(T) \pm C \exp[-t R(T)], \tag{2}$$

where C is proportional to the defect concentration, with a positive sign consistent with minority carrier emission and a negative sign indicating majority carrier emission. The sign of C is the strength of the capacitance-based DLTS technique. Similar current–transient-based techniques cannot distinguish between minority carrier or majority carrier emissions, because each carrier contributes identically to any current measured [20–22].

The constant value B is not a function of time, only of temperature, and represents the case of complete defect ionization. In practice, the temperature dependence of the background signal, $B(T)$, complicates transient analysis because, a priori, it is not known whether the background is a constant or a very slowly ionizing defect site. The SLAP methodology presented below effectively removes this ambiguity.

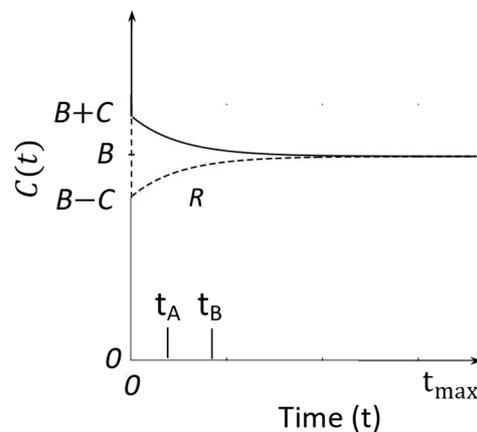


Figure 1. DLTS capacitance transients for minority carriers (solid line) and majority carriers (dashed line), following the removal of a fill pulse at time $t = 0$. t_A and t_B represent sampling times for a waveform sampled for a total time, t_{max} .

Traditionally, the capacitance transients of DLTS were repeated and averaged using an analog boxcar average [1]. The double-boxcar average technique was configured to sample a repeated input signal at two chosen times, t_A and t_B , which define a rate window. This

analog gated measurement was synchronized with the start of defect ionization, producing a derived signal, as follows:

$$DLTS(t_A, t_B, T) \equiv C(t_B, T) - C(t_A, T). \quad (3)$$

Then, for traditional capacitance-based DLTS, temperature is slowly swept, and a peak in the DLTS signal is found at some temperature, T_{peak} , when the emission rate is given by

$$R(T_{\text{peak}}) = \frac{\ln\left(\frac{t_B}{t_A}\right)}{t_B - t_A}. \quad (4)$$

The double-boxcar average output is then plotted versus temperature to produce a set of $T_{\text{peak},i}$, each of which defines an emission rate, R_i , for the i th defect, according to Equation (4). Each $T_{\text{peak},i}$ contributes to the spectral signature unique to the type (donor or acceptor), concentration, capture parameter, and ionization energy of all defects present. Analysis of a DLTS signal deconvolves this signature into an integer number of specific defects. Because traditional capacitance-based DLTS requires a temperature scan to determine the temperature which maximizes the DLTS signal, each data point requires the system to first come into temperature equilibrium with its surroundings, followed by any signal averaging required to improve the signal-to-noise ratio. This effort produces a single point of the traditional DLTS, the temperature domain spectrum. The SLAP methodology also requires the temperature to equilibrate followed by signal averaging to improve the signal-to-noise ratio. However, the SLAP transform algorithm effectively searches for that rate window which will maximize the SLAP signal at the current temperature, with minimal computational overhead. Thus, the SLAP methodology can produce a full rate domain spectrum in the time it takes to produce one point of a DLTS temperature domain spectrum.

Although relatively simple for a single defect, the challenge is to resolve the signatures of multiple defects, whose concentration, type, and ionization parameters are unknown [2–7,23–26]. In traditional boxcar-based, temperature-swept DLTS, two neighboring peaks can be distinguished if their emission rates differ by at least ~8 times [6]. Other, more recent DLTS analysis techniques utilize the Laplace transform (L-DLTS) or Fourier transform (deep-level Fourier spectroscopy) to improve signal acquisition and rate extraction to improve emitter distinguishability [6,7,23]. Both techniques are constant-temperature approaches, such as the SLAP technique, allowing for unlimited signal averaging for improved signal-to-noise ratio. Both techniques offer improvements over the original double-boxcar technique in that the judgment of the user is not required to determine peak location in temperature or rate, instead relying on curve-fitting algorithms to obtain peak location and height, sharing a similar strength with the proposed SLAP technique. Both L-DLTS and deep-level Fourier spectroscopy identify defects as a spectral feature, as does SLAP, with the SLAP technique offering minimal computational overhead and a simple curve-fitting function for peak characterization. Significantly, both L-DLTS and Fourier spectroscopy are based on integrals summed from zero to infinity. This is in stark contrast to the SLAP technique, which obtains results as an integer sum with each integer representing a unique defect. As will be shown, the SLAP technique also provides both minority and majority carrier defect information from a single transient. In all cases, a constant-temperature approach is used for more precise determination of defect parameters through signal averaging, with a signal-to-noise ratio of at least 1000 required for Laplace DLTS to provide better rate resolution than offered by the traditional double-boxcar DLTS technique [23].

3. Results

We present a mathematical “sliding-aperture” transform (or SLAP) to obtain defect parameters from capacitance transients measured at constant temperature. Each capacitance transient is an integer sum over k defect species of exponential transients, Equation (2), each with its own set of parameters, C_i , and R_i , where the subscript “ i ” enumerates the defects.

For any fixed temperature, there is a single constant offset, B , corresponding to the quiescent reverse bias capacitance value at infinite time when all defects have been ionized. The SLAP transform is plotted as a function of the rate variable $\rho = 1/t$ and produces a defect signature composed of a set of peaks whose locations identify the rates R_i , and whose peak values define the peak capacitances C_i . Spectra taken at different fixed temperature will have defect signatures shifted to different positions on the ρ axis, according to Equation (1). Analysis of the temperature dependence of the obtained R_i values then gives the desired defect parameters E_i and P_i . Like traditional DLTS, the background, B , subtracts out and needs to be determined by other means to accurately determine defect concentration from the transient maximum.

The SLAP transform is defined as

$$SLAP(\rho) \equiv C\left(\frac{N}{\rho}\right) - C\left(\frac{1}{\rho}\right), \tag{5}$$

where all quantities are evaluated at the same constant temperature and the SLAP function is expressed in terms of the rate variable $\rho = 1/t$. The aperture N is defined as

$$N = \frac{t_B}{t_A}, \tag{6}$$

where t_A represents the first sampled time after the removal of the fill pulse. In the simplest case, for a transient sampled at a fixed sampling period, the first few ordered pairs of the SLAP transform for the $N = 2$ case will be:

$$\begin{aligned} &\left(\frac{1}{t_A}, C(2t_A) - C(t_A)\right) \\ &\left(\frac{1}{2t_A}, C(4t_A) - C(2t_A)\right) \\ &\left(\frac{1}{3t_A}, C(6t_A) - C(3t_A)\right) \\ &\vdots \\ &etc. \end{aligned}$$

Any waveform, sampled at a fixed sampling rate, can be SLAP-transformed using the above algorithm. This work concentrates on the special case, where the original function is of the form of Equation (2), namely a decaying exponential plus a constant baseline. This leads to the following SLAP function:

$$SLAP(\rho) \equiv \pm C \left[\exp\left(-N \frac{R}{\rho}\right) - \exp\left(-\frac{R}{\rho}\right) \right]. \tag{7}$$

Transforming a digital waveform, as described above, will lead to a waveform that can be curve-fit with the SLAP function of Equation (7). Alternatively, the SLAP function of Equation (7) can be used as an equivalent representation of the decaying exponentials of Figure 1 with the constant background, $B(T)$, eliminated, as shown in Figure 2. Here, a positive and a negative SLAP peak are plotted in the inverse time, or rate domain ρ , on axis, with the axis scaled by factors notated as σ_x and σ_y . These scale factors are obtained by first noting that the SLAP peak will be located at R , where,

$$R = \frac{\ln(N)}{N-1} \rho_{peak} = \sigma_x \rho_{peak}. \tag{8}$$

with direct substitution of Equation (8) into (7) leading to

$$C = SLAP_{peak} / [\exp(-N\sigma_x) - \exp(-\sigma_x)] = SLAP_{peak} / \sigma_y, \tag{9}$$

which defines both the σ_x and σ_y scaling factors.

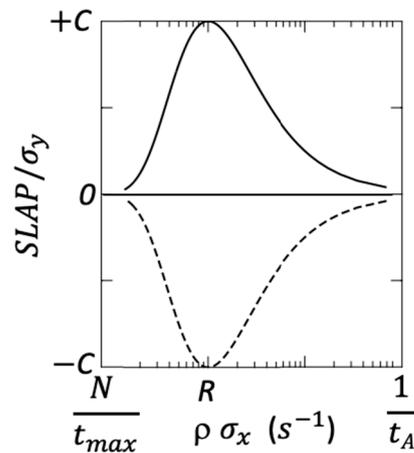


Figure 2. SLAP transformation of the decaying exponentials of Figure 1.

In general, each defect species is characterized by the physical attributes associated with Equation (1), namely emission rate and capture parameter. This leads to the SLAP transformation for multiple emitters as an integer sum of the following form:

$$SLAP(\rho) = \sum_{i=1}^k \frac{\pm C_i}{\sigma_y} \left[\exp\left(-N \frac{R_i \sigma_x}{\rho}\right) - \exp\left(-\frac{R_i \sigma_x}{\rho}\right) \right] \tag{10}$$

which produces k peaks, each of which defines a pair of defect parameters (R_i, C_i).

The strength of the SLAP approach to transient analysis is the ability to use Equation (10) and a simple curve-fitting algorithm to curve-fit a multipeak spectrum based on an integer number of defects. This removes user intervention from the process of rate and peak height determination and is not only the strength of this work but is prominent attribute for both L-DLTS and deep-level Fourier spectroscopy [6,7,23]. SLAP offers another means of characterizing defect spectrum through the sequential use of Equation (10), first under the assumption of a single defect (i.e., $i = 1, k = 1$), followed by the introduction of more defect species (i.e., $k > 1$).

This algorithm is now used to assess the effect of noise on rate and maximum value extraction from simulated noise-loaded transients using Equation (10). The simultaneous ionization of two majority and one minority defect species, the SLAP transforms of which are shown individually in Figure 3, were summed and simulated with noise added. Signal-to-noise ratios, S/N , of 20, 50, and 1000 were investigated, with the superposition in the worst-case $S/N = 20$ plotted in Figure 4. Curve-fitting was proceeded by assuming one-four defects with unconstrained signs for the C_i . For all simulations a sampling period of 0.2 s^{-1} was used with 10^5 sampled points. Convergence was obtained in cases of one-three defects with results shown. No convergence or vanishingly small C_i values were obtained in the four-defect case. The three-defect case gave the best fit for all S/N considered. When $S/N = 1000$, the obtained defect parameters (R_i, C_i) were the same as indicated in Figure 2 within 1%. When $S/N = 20$, obtained values of (91, +0.7), (176, -0.46), and (496, 0.51). These values differ from the input values by (9, 30), (17, 39), and (1, 2)%, respectively. The simulations suggest that SLAP peaks can be resolved when $S/N = 1000$ if their rates differ by as little as a factor of 1.5.

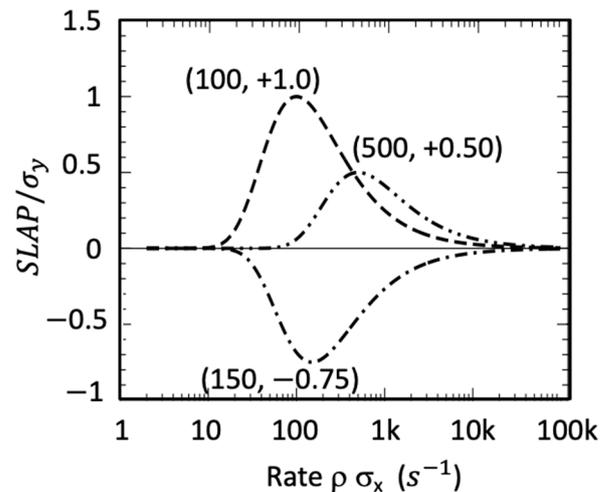


Figure 3. SLAP transforms of two majority and one minority carrier defects with decay rates and maximum values shown as ordered pairs.

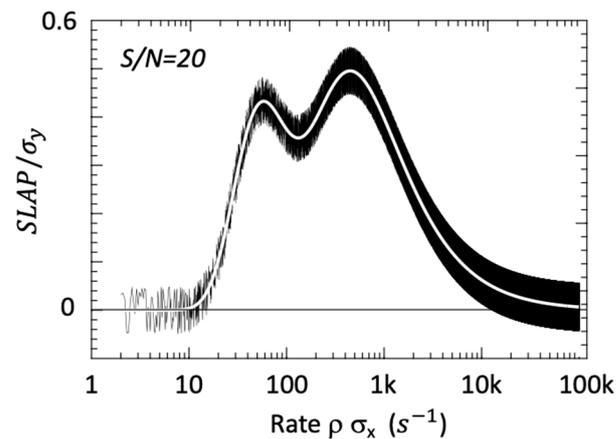


Figure 4. Superposition of SLAP peaks with added noise ($S/N = 20$) and best fit assuming three defects.

4. Discussion

We introduced the SLAP transform as a means to deconvolve the multiexponential capacitance transients often observed during DLTS investigations of defects in semiconducting materials. Its application to the analysis of noise-laden capacitance transients at constant temperature was used to illustrate the strength of the derived SLAP function as an aid in the determination of the type, decay rate, maximum value, and number of each emitter present. This work suggests the SLAP transform should provide exceptionally high resolving power to distinguish defects with ionization rates different by as little as 1.5 for signal-to-noise ratios of 1000.

SLAP may be applied to determine rate constants for other types of decays. For instance, it has recently been used in the analysis of laser propagation decay in scattering media [27]. This work neatly demonstrates the value of SLAP to determine decay constants when there is an unknown background.

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